GEOTECHNICAL INVESTIGATION OF SLAB MOISTURE INTRUSION BRIDGEPORT ELEMENTARY SCHOOL (SAUGUS UNION SCHOOL DISTRICT)

23670 Newhall Ranch Road Santa Clarita, California

July 19, 2017 FN 05725-01



Corporate Office: 22725 Old Canal Rd. Yorba Linda, CA 92887

2640 Financial Court Suite A San Diego, CA 92117 3100 Fite Circle Suite 103 Sacramento, CA 95827 5600 Spring Mtn. Rd. Suite 201 Las Vegas, NV 89146





July 19, 2017

File No. 05725-01

Ms. Lynn Beekman FAGEN FRIEDMAN & FULFROST LLP 1525 Faraday Avenue, Suite 300 San Diego, California 92008

Project: <u>GEOTECHNICAL INVESTIGATION OF SLAB MOISTURE INTRUSION</u> BRIDGEPORT ELEMENTARY SCHOOL (SAUGUS UNION SCHOOL DISTRICT) 23670 Newhall Ranch Road Santa Clarita, California 91355-1640

Dear Ms. Beekman:

As requested, American Geotechnical has performed a geotechnical investigation of the suspected slab moisture intrusion concerns at the Bridgeport Elementary School in Santa Clarita, California. This report presents our investigation findings. The investigation included the following scope of work.

- Review of documents pertaining to the site construction and reported moisture intrusion that were provided to us. Documents reviewed are listed in **Appendix A**.
- Visual review of the site conditions within the building interiors and the exterior school grounds. Photographs of observed conditions are presented in **Appendix B.**
- Moisture dome (vapor emission) testing of the interior concrete slabs in three school rooms at 11 locations utilizing the moisture dome test method. The approximate locations of the moisture dome tests and photographs are presented in **Appendix C**.
- Exploratory coring through the concrete slab-on-grade and sampling of the underlying soil in each of the three rooms that were tested for slab vapor emission rates. The approximate core locations are shown on the moisture dome test location maps in Appendix C. Field logs and photographs of the exploratory cores are presented in Appendix D.
- Two exploratory hand-auger borings with soil sampling and installation of two shallow groundwater monitoring wells (piezometers), and groundwater depth measurements were taken in the piezometers. The approximate locations of the hand-auger borings/piezometers are shown on Figure 1. Field logs and photographs of the exploratory hand-augers for the piezometer installations are presented in Appendix D.

File No. 05725-01 July, 19, 2017 Page 2

- Laboratory testing of soil samples collected from the exploratory corings and hand-auger borings. Soil testing included intact moisture content and density, and soil classification. Laboratory measurements of the slab cores were also performed. The laboratory test results are presented in Appendix E.
- Engineering and geologic analysis of the data acquired from the investigation.
- Preparation of this written report summarizing our findings.

### 1.0 SITE DESCRIPTION AND REPORTED DISTRESS

The Bridgeport Elementary School is located at 23670 Newhall Ranch Road in the City of Santa Clarita, California. The school has a central cluster of connected buildings surrounded by several detached classroom buildings to the west and southwest, and a common area concrete courtyard and asphalt sports courts to the east and southeast (see **Figure 1**). There are four lawn planter areas located between the central building cluster and detached classrooms on the west side. The sod areas are relatively flat and level, and are surrounded by concrete flatwork. The sod areas have restricted drainage directed towards surface area drains located approximately in the middle of each lawn area. The school was constructed in two phases and we were provided the Phase 1 construction plans to review. The school was built more than 10 years ago but sometime after 2001, which is the date of the Phase 1 structural plans that we reviewed. The school buildings are supported on conventional concrete slab-on-grade foundations. According to the foundation plans prepared by Thompson & La Brue Structural Engineers, the interior slabon-grade foundations were specified to be 4-inches thick and reinforced with No. 4 steel bars placed at least 1-inch below the slab surface and spaced 18-inches apart in both directions. The slabs were also to be underlain by a 6-mil Visqueen vapor barrier overlain and underlain with 2 inches of sand (4-inch total thickness). The concrete specifications called for 2500 psi concrete for slabs and 3000 psi concrete for footings.



Geotechnical, Bridgeport Elementary 1 Inc. School	American	Test Location Plan	Figure
EN 5725.04 Santa Clarita Ca	Geotechnical, Inc.	Bridgeport Elementary School	1
F.N. 5725.01 Santa Clainta, Ca	F.N. 5725.01	Santa Clarita, Ca	

File No. 05725-01 July, 19, 2017 Page 3

The Phase 1 construction plans specify that the floor finishes for the central school building and the detached kindergarten classroom were to consist of carpet, linoleum tile, ceramic tile, quarry tile, and sealed concrete. According to the plans, both of the rooms that we tested in the central school building, (rooms 11 & 31), were initially finished with carpet. Reportedly, at some point the flooring in some of the classrooms began to emit an offensive odor. Some of the original flooring was then replaced with carpet that was glued to the slab with a mastic adhesive in an attempt to seal the slab, but then the mastic adhesive apparently failed. The flooring was then replaced again with rubber-backed carpet tiles that were spot-glued in place. However, reportedly some of the classrooms continued to be affected by an offensive odor possibly caused by moisture intrusion and/or carpet tile backing glue degrading in the presence of moisture. It is our understanding that Exponent, Inc. conducted an indoor air quality investigation and conducted emissions testing on carpet tile samples at Bridgeport Elementary. Our further understanding is that Exponent, Inc. issued two reports that outlines the findings from the investigations (See References in **Appendix A**). In May of 2017, American Geotechnical was asked to perform an investigation of the suspected moisture intrusion problem and provide recommendations for improvement.

### 2.0 SITE OBSERVATIONS

We observed the conditions of the interior flooring of the school rooms affected by suspected moisture intrusion and the adjacent exterior school grounds. Some of the square carpet tiles were removed to expose the underlying slab. At several locations we observed visible condensation on the rubber backing of the underside of the carpet tiles. Condensate staining was also observed on the concrete slab surface beneath the carpet, and remnants of the old mastic adhesive from the previous carpeting were also seen at many locations.

The courtyard located between the central school building complex and the detached classrooms located to the west contains concrete flatwork surrounding four lawn areas. The lawn areas have one or more surface drains located approximately in the center of each lawn area to capture runoff. At the time of our initial site visit it had been raining a day or two before our arrival. The court yard walkway areas between lawn areas had standing water present. Apparently this is a recurring problem after rain events. The surface drainage in the court yard appears to be inadequate to accommodate runoff during periods of heavy rainfall.

File No. 05725-01 July, 19, 2017 Page 4

#### 3.0 CONCERTE MOISTURE DOME (VAPOR EMISSION) TESTING

The concrete slab foundation was tested for moisture vapor emission in three school rooms, which included the teacher staff room A31, and the classrooms A11 and C1 (see **Figure 1** for classroom locations). The moisture dome test method was utilized to measure the moisture vapor emission rate of the slab surface in general conformance with ASTM Standard F-1869. A total of 11 tests were performed. However, one of the moisture domes was disturbed during the test period, which invalidated the test results at that location. The remaining 10 tests yielded moisture vapor emission rates ranging from 4.2 to 8.5 lbs per 1,000 square feet of floor area per day. The average moisture vapor emission rate for all 10 tests was 6.34 lbs per 1,000 square feet per day. The test results are presented in **Table 1**. The measured vapor emission rates are higher than the maximum allowable value of 3-5 lbs per 1,000 square feet per day specified by most flooring manufacturers.

### 4.0 CONCRETE SLAB CORINGS

The concrete slab-on-grade foundation was cored at one location within each of the three school rooms tested for vapor emission rates. A concrete coring subcontractor was hired to core through the slab with a 6-inch diamond bit coring machine. American Geotechnical supervised the coring and then logged and sampled the slab and the underlying soil conditions. Intact and bulk soil samples were collected from each core hole to a maximum depth of 31 inches below the slab surface. Field measurements of the slab thickness at the core locations ranged from a minimum of about 4.125 inches to a maximum of about 5.25 inches, which is more than the 4-inch thickness specified on the structural plans that we reviewed. We found the slabs to be reinforced with ½ -inch steel rebar set within the middle or lower third of the slab thickness and spaced at about 11 to 18-inches apart in both directions. The slabs were underlain with a moisture barrier consisting of an upper layer of sand placed on top of a yellow plastic sheet overlying another sand layer. The upper layer of sand was approximately 2-inches thick and the lower sand layer was generally only about 1-inch thick. The yellow plastic vapor barrier sheet appeared to be a Stegowrap product. The soil underlying the slab generally consisted of silty Sand with some cobbles and variable amounts of minor clay, and was relatively dense and moderately moist. Field logs of the cores are presented in **Appendix D**.

File No. 05725-01 July, 19, 2017 Page 5

#### 5.0 HAND-AUGER BORINGS/PIEZOMETERS

Two hand auger borings were advanced through the lawn areas within the court yard located west of the central building complex (see **Figure 1** for approximate locations) and piezometer pipes (groundwater monitoring wells) were installed in the boreholes. The piezometers consisted of 1.5-inch diameter slotted pipe backfilled with a permeable sand pack and capped with an impermeable bentonite surface seal. Soil samples were collected and the conditions were logged as the hand-augers were advanced. The first hand-auger was advanced to a depth of just over 10 feet. Cobbles were encountered in the second hand-auger that prevented its advancement beyond a five foot depth. The soil conditions encountered in the hand-augers were generally similar to those encountered beneath the slab cores. Field logs of the exploratory hand-augers for the piezometer installations are presented in **Appendix D**.

Seepage and perched groundwater was encountered at about 7-feet depth in the first hand-auger boring (AGPZ-1), but no seepage or groundwater or seepage was encountered during advancement of the second hand-auger (AGPZ-2). A groundwater depth reading was taken from AGPZ-1 after installation and the depth of the groundwater was approximately 7.6 feet inside the pipe. The piezometer was then bailed to lower the water level inside the pipe so that it could recharge to a stabilized depth before any additional readings were taken. Both piezometers were read again the following day and the groundwater depth had risen to about 6.52 feet inside the AGPZ-1, but no groundwater was found in AGPZ-2. The groundwater inside AGPZ-1 was bailed again to lower the water inside the pipe to a depth of 9.22 feet before leaving the site. A third reading of both piezometers was taken three days later and at that time the groundwater depth in AGPZ-1 was 8.3 feet. Groundwater was also found in AGPZ-2 at a depth of 3.75 feet during the third reading. The groundwater measured in AGPZ-2 was likely from irrigation water that seeped into the piezometer from the surface. The piezometers were read again on July 10, 2017. The depth of the groundwater in AGPZ-1 was 6.60 feet and AGPZ-2 was dry.

File No. 05725-01 July, 19, 2017 Page 6

#### 6.0 LABORATORY TESTING

Intact and bulk soil samples collected from the exploratory core holes and hand-auger borings were transported to our office for laboratory testing. Tests performed included field moisture content and density, and soil classification. Laboratory measurements of the slab cores were also performed.

The soil samples collected from the hand-auger borings classified as silty to clayey Sand. The moisture contents of the samples collected from the fill material beneath the slabs ranged from 7.7 to 10.5 percent, with an average of 9.5 percent. The degree of saturation of these samples ranged from 56 to 75 percent, with an average of 70 percent. The moisture contents of the samples collected from the hand-auger borings ranged from 7.9 to 13.7 percent, with an average of 11.0 percent. The degree of saturation for the auger soil samples ranged from 47 to 92 percent, with an average of 71 percent. The moisture contents and degrees of saturation were slightly higher on average for the auger soil samples than the core soil samples likely due to irrigation water percolating into the landscape areas. The average thickness of the three slab cores as determined by laboratory measurements was 4.8 inches, and the plastic vapor barrier was measured to be 15 mils thick. Summaries of the laboratory test results are presented in **Appendix E**.

### 7.0 <u>CONCLUSIONS</u>

The results of the moisture vapor emission testing performed on the three school rooms indicate that the slabs are being affected by elevated rates of moisture vapor transmission through the slab surface. The excessive moisture vapor appears to be primarily caused by moisture from the sub-slab soil being transmitted through the slabs due to relatively permeable concrete (2500 psi) and normal pressure differentials. The low compressive strength (2500 psi) of the concrete selected in the specification created a condition conducive to higher levels of moisture vapor emissions.

The area has experienced drought conditions for several years with very little measurable rainfall. On the other hand, irrigation levels to sustain sod areas within the courtyards and playing fields at the school are quite substantial and occur on a more regular basis over time. The irrigation water accumulates over time, which creates "moist" soil conditions. Groundwater is not considered to be a factor contributing to the excessive moisture vapor emissions.

File No. 05725-01 July, 19, 2017 Page 7

The moisture vapor that is being transmitted through the concrete slab is being trapped beneath the relatively impermeable rubber-backed carpet flooring, causing it to condense and stain the slab surface and carpet, and apparently creating an offensive odor at many locations. Exponent's report found that the odors were likely caused by moisture under the carpets and the degradation of carpet tile backing or glue.

Slab moisture vapor emission is driven by vapor pressure differentials between the interior conditions of an enclosed building and the exterior conditions within and beneath the concrete slab. The dryer, lower atmospheric pressure conditions within enclosed air conditioned buildings causes moisture in the form of moisture vapor to migrate through the concrete slab from the more humid conditions that occur within and beneath the slab. Vapor transmission will continue to occur indefinitely as long as a vapor pressure differential exists between the interior and exterior conditions of a building. Vapor emission rates higher than 3.0 lbs per 1000 square feet over a 24 hour period can adversely affect many floor coverings. A vapor retarder such as the plastic sheeting found underlying the concrete slabs of the school rooms can reduce the amount of moisture vapor transmitted from the soil, but it is not completely effective in controlling vapor emissions.

### 8.0 **RECOMMENDATIONS**

To reduce the rate of vapor emission being transmitted through the concrete slabs we recommend that the slab surfaces be treated with a high quality topical sealant. The treatment should include removal of the interior floor coverings and preparation of the slab surface by bead-blasting to remove all deleterious materials and abrade the concrete surface to ensure a good bond is formed with the sealant. All existing slab cracks or joints should also be sealed with pressure-injected epoxy or a low viscosity gravity fill epoxy before the topical slab sealant is applied.

The slab surface should be cleaned and prepared, and the slab sealant should be applied in strict accordance with the manufacturer's specifications and procedures by an experienced, licensed, and qualified contractor. Also, after treatment the slab sealant is typically covered with a protective coating to prevent it from being damaged and compromised prior to the installation of new floor coverings. It is our understanding that Ralph Godfrey of R. Godfrey Consulting has developed the specifications for slab sealant and is also currently in the process of meeting with floor sealant contractors in an effort to complete the project by the end of summer. If additional information is needed to aid in carrying out the remedial process, our office can be contacted.

File No. 05725-01 July, 19, 2017 Page 8

In addition to the slab sealant remediation process, the exterior landscape areas surrounding the buildings should have positive drainage directed away from the foundations to prevent percolation of water into the subgrade. Any areas where ponding occurs next to buildings should be improved to provide positive drainage away from the foundations. This could require the installation of additional surface drain inlets in hardscape and landscape areas wherever the existing drainage is inadequate to prevent runoff form ponding at the surface. Subsurface drains are not considered necessary based on water levels observed through our monitoring and investigation. Irrigation of landscape areas should be checked and maintained to ensure that only enough water is being applied to sustain the landscape vegetation to prevent overwatering and percolation of excess irrigation water into the subgrade. As discussed at the site, consideration should be given to convert landscape areas to drought-tolerant, low-water landscaping.

#### 9.0 LIMITATIONS

Conclusions and recommendations presented herein are based on evaluations of technical information gathered, experience and professional judgment. Other consultants could arrive at different opinions and conclusions. Subsurface conditions can often vary across a given site; therefore conditions may differ at locations not tested. American Geotechnical did not design or construct any portion of the site and therefore we cannot provide any guarantee of its future performance. If additional information concerning the site becomes available it should be forwarded to our office for review so that we can revise our opinions and recommendations if needed. The contents of this report are presented for the sole benefit of the client and should not be used by any other parties without the client's permission.

Typically, "minimum" recommendations have been presented. Although some risk will always remain, lower risk of future problems would usually result if more restrictive criteria were adopted. Final decisions on matters presented are the responsibility of the client and/or the governing agencies. No warranties in any respect are made as to the performance of the project.

File No. 05725-01 July, 19, 2017 Page 9

We appreciate the opportunity to be of service. If you should have any questions or concerns, please do not hesitate to contact this office.

Sincerely,

AMERICAN GEOTECHNICAL, INC.

Edred T. Marsh Principal Engineer G.E. 2387

KR/ETM: am

Distribution: Ms. Lynn Beekman – (1)



Roge Kani R.

Kevin R. Rogers Chief Geologist C.E.G. 2425



Via Email

Bridgeport Elementary File No. 05725-01

### American Geotechnical, Inc.

#### Table 1 - Vapor Emissions Test Results

Moisture Dome No.	Room	RoomTest Start DateTest Start TimeInitial 							Vapor Emission Volume in Ibs. / 1000 sq. ft. in 24 hours						
MD-1	A31	06/04/17	8:30	73.0	57.0	4.0, 4.5, 4.5, 4.3	33.6	06/07/17	6:00	37.5	68.5	53.0	3.9	69.50	6.6
MD-2	A31	06/04/17	8:37	73.0	56.0	4.0, 4.1, 4.0, 4.2	32.4	06/07/17	6:01	35.8	69.0	53.0	3.4	69.40	5.8
MD-3	A31	06/04/17	8:40	73.0	55.0	3.9, 3.8, 3.1, 3.1	33.5	06/07/17	6:03	-	69.9	52.0	0.0	69.38	N/A
MD-4	A11	06/04/17	8:48	74.0	54.0	4.5, 4.2, 4.6, 4.4	34.3	06/07/17	6:10	38.4	71.0	50.0	4.1	69.37	7.0
MD-5	A11	06/04/17	8:53	74.0	55.0	4.2, 4.3, 4.2, 4.6	32.8	06/07/17	6:15	37.2	71.4	49.0	4.4	69.37	7.5
MD-6	A11	06/04/17	8:59	74.0	56.0	4.2, 4.2, 3.5, 4.1	32.9	06/07/17	6:19	37.9	71.2	49.0	5.0	69.33	8.5
MD-7	A11	06/04/17	9:03	74.0	56.0	4.2, 4.2, 3.8, 4.0	33.7	06/07/17	6:24	37.5	71.2	50.0	3.8	69.35	6.4
MD-8	C1	06/04/17	9:10	73.0	51.0	3.9, 4.0, 3.8, 3.9	33.8	06/07/17	6:29	36.6	71.4	50.0	2.8	69.32	4.8
MD-9	C1	06/04/17	9:16	73.0	56.0	4.5, 4.8, 4.3, 3.4	33.1	06/07/17	6:33	36.6	71.7	48.0	3.5	69.28	5.9
MD-10	C1	06/04/17	9:20	73.0	58.0	3.3, 3.0, 3.6, 3.5	33.4	06/07/17	6:36	35.9	71.5	48.0	2.5	69.27	4.2
MD-11	C1	06/04/17	9:25	73.0	61.0	4.3, 4.5, 4.3, 4.5	30.1	06/07/17	6:41	34.0	71.5	48.0	3.9	69.27	6.7
													<u>Standar</u> <u>Avg. +</u> <u>Avg. + 1.28</u>	<u>6.34</u> <u>2.24</u> <u>8.58</u> <u>9.21</u>	



### **APPENDIX A – DOCUMENTS REVIEWED**

"Bridgeport Elementary School - Phase 1" Architectural plans prepared by PSWC Group Architects/Planners, dated 12-1-99.

"Bridgeport Elementary School - Phase 1" Structural plans prepared by Thompson & La Brie Structural Engineers, dated 01-10-2001.

"Indoor Air Quality Investigation, Bridgeport Elementary School, 23670 Newhall Ranch Road, Valencia, California, Exponent Project No. 1703766.00," prepared by Exponent, Inc., dated May 23, 2017

"Volatile Organic Compound (VOC) Emissions from Select Installed Carpet Tiles, Bridgeport Elementary School, 23670 Newhall Ranch Road, Valencia, California, Exponent Project No. 1703766.00," prepared by Exponent, Inc., dated May 30, 2017



### **APPENDIX B – SITE PHOTOGRAPHS**

American Geotechnical, Inc. FILE NO: 05725.01 PROJECT: Bridgeport Elementary School DESCRIPTION: Classroom A-11 AGMD 4-6 12/17 6 DATE: SHEET: 1.0.1 AGMD-4 Exterior Interior Door Door 6.2' 109 AGMD.6 18.4 20.2 AGMD-5 AGMD-7K \* 4.2' Photos (35) DPlaque z) Classroom # 3)-5) AGMD-4 OV before prep (x)-8) AGMD-50V before prep (A)-11) AGMD - 6 OV before prep





Mositure Dome Prep, A11 - JS 6-3-17 (1)



Mositure Dome Prep, A11 - JS 6-3-17 (2)





Mositure Dome Prep, A11 - JS 6-3-17 (3)



Mositure Dome Prep, A11 - JS 6-3-17 (4)





Mositure Dome Prep, A11 - JS 6-3-17 (5)



Mositure Dome Prep, A11 - JS 6-3-17 (6)





Mositure Dome Prep, A11 - JS 6-3-17 (7)



Mositure Dome Prep, A11 - JS 6-3-17 (8)





Mositure Dome Prep, A11 - JS 6-3-17 (9)



Mositure Dome Prep, A11 - JS 6-3-17 (10)





Mositure Dome Prep, A11 - JS 6-3-17 (11)

American Geotechnical, Inc. FILE NO: 05725-01 PROJECT: Bridgeport Elementary School Teacher's Lounge AGMD1-3 DESCRIPTION:\_ DATE: 6/2/13 SHEET: BY: AGM0 - 1 inside door 8.9 13.4 outside AGC-1 en brance AGMD-3 14.6 2.2' rAGMD-Z Photos (JS) D Plaque z) Outside OV 3) Outside door 4) Outside OV 5)-9) AGMD-1 OV before prep 10- 12) AGMD-2 OV before piep 13)-15) AGMD-3 OV balore prep 16)-17) 1" slab ek, exposed after prep (800) 275-4436 • WWW.AMGT.COM •





Mositure Dome Prep, A31 - JS 6-3-17 (1)



Mositure Dome Prep, A31 - JS 6-3-17 (2)





Mositure Dome Prep, A31 - JS 6-3-17 (3)



Mositure Dome Prep, A31 - JS 6-3-17 (4)





Mositure Dome Prep, A31 - JS 6-3-17 (5)



Mositure Dome Prep, A31 - JS 6-3-17 (6)





Mositure Dome Prep, A31 - JS 6-3-17 (7)



Mositure Dome Prep, A31 - JS 6-3-17 (8)





Mositure Dome Prep, A31 - JS 6-3-17 (9)



Mositure Dome Prep, A31 - JS 6-3-17 (10)





Mositure Dome Prep, A31 - JS 6-3-17 (11)



Mositure Dome Prep, A31 - JS 6-3-17 (12)





Mositure Dome Prep, A31 - JS 6-3-17 (13)



Mositure Dome Prep, A31 - JS 6-3-17 (14)





Mositure Dome Prep, A31 - JS 6-3-17 (15)



Mositure Dome Prep, A31 - JS 6-3-17 (16)





Mositure Dome Prep, A31 - JS 6-3-17 (17)

American Geotechnical, Inc. FILE NO: 05725, 01 PROJECT: Bridge port Elementary School DESCRIPTION: Classroom C1 AGMD 7-9 6/2/13 JS BY: \_\_\_\_\_ DATE: SHEET: 39 AGMD-B AGMD-11 outside 12.3 door 14.6 AGMD-P EAGC-3 167 1.9' AGMD-9 ×1.0! Photos (FS) D Plaque z) C1 door plaque z) AGMD - 7 OV before prep 4) 5) 11 6)-8) AGMO-8 OV before prep





Mositure Dome Prep, C1 - JS 6-3-17 (1)



Mositure Dome Prep, C1 - JS 6-3-17 (2)





Mositure Dome Prep, C1 - JS 6-3-17 (3)



Mositure Dome Prep, C1 - JS 6-3-17 (4)





Mositure Dome Prep, C1 - JS 6-3-17 (5)



Mositure Dome Prep, C1 - JS 6-3-17 (6)





Mositure Dome Prep, C1 - JS 6-3-17 (7)



Mositure Dome Prep, C1 - JS 6-3-17 (8)




Moisture Domes - KR 6-4-17 (1)



Moisture Domes - KR 6-4-17 (2)





Moisture Domes - KR 6-4-17 (3)



Moisture Domes - KR 6-4-17 (4)





Moisture Domes - KR 6-4-17 (5)



Moisture Domes - KR 6-4-17 (6)





Moisture Domes - KR 6-4-17 (7)



Moisture Domes - KR 6-4-17 (8)





Moisture Domes - KR 6-4-17 (9)



Moisture Domes - KR 6-4-17 (10)





Moisture Domes - KR 6-4-17 (11)



Moisture Domes - KR 6-4-17 (12)





Moisture Domes - KR 6-4-17 (13)



Moisture Domes - KR 6-4-17 (14)





Moisture Domes - KR 6-4-17 (15)



Moisture Domes - KR 6-4-17 (16)





Moisture Domes - KR 6-4-17 (17)



Moisture Domes - KR 6-4-17 (18)





Moisture Domes - KR 6-4-17 (19)



Moisture Domes - KR 6-4-17 (20)





Moisture Domes - KR 6-4-17 (21)



Moisture Domes - KR 6-4-17 (22)



#### **APPENDIX B – SITE PHOTOGRAPHS**





Site Review - ETM 5-16-17 (1)



Site Review - ETM 5-16-17 (2)





Site Review - ETM 5-16-17 (3)



Site Review - ETM 5-16-17 (4)





Site Review - ETM 5-16-17 (5)



Site Review - ETM 5-16-17 (6)





Site Review - ETM 5-16-17 (7)



Site Review - ETM 5-16-17 (8)





Site Review - ETM 5-16-17 (9)



Site Review - ETM 5-16-17 (10)





Site Review - ETM 5-16-17 (11)



Site Review - ETM 5-16-17 (12)





Site Review - ETM 5-16-17 (13)



Site Review - ETM 5-16-17 (14)





Site Review - ETM 5-16-17 (15)



Site Review - ETM 5-16-17 (16)





Site Review - ETM 5-16-17 (17)



Site Review - ETM 5-16-17 (18)





Site Review - ETM 5-16-17 (19)



Site Review - ETM 5-16-17 (20)





Site Review - ETM 5-16-17 (21)



Site Review - ETM 5-16-17 (22)



#### **APPENDIX C – VAPOR EMISSION TEST & CORE LOCATION MAPS & PHOTOGRAPHS**



#### **APPENDIX D – SUBSURFACE LOGS & PHOTOGRAPHS**



#### **APPENDIX D – SUBSURFACE LOGS & PHOTOGRAPHS**

Coring No. Project Name: Location: <u>Ro</u>	AGC Brid	-1 geport Ele A31 (sta	mentary ff weeti	School my room)	File No. Sheet: Start Date:	June 3, Z
Total Depth:	30/4	Rig Type: _ <u>(</u>	6" Core M	<u>Ach</u> . Est. Surface	e日evation:	
Depth in Feet Type	Sample Depth	Surface Conditions Subsurface Condition	Field Desc	ATION: Classification, co	By: ,	ghtness, etc.
		0-41/2 (sh # 4 reba E-w d 1 41/2-71/4 SI tan, mo 71/4 Yellow possibly 71/4-81/4 SA 81/4-301/4 gravel	C. Core 6 W/in botton 1" to 14" april 1" to 14" april 100 BLANKE STEGO N PND BLANK FILL SOHA OKSYWO	dia. × 43/8/ n fhird of st art N-5, T siffy SANE coring mach.) zet Vapor bar NRAP produce SAND W/UC to Med bru	Min 51/4 as space w/f.grav Med.d rier hea t as=ve uriable ( wn, mois	"Max thick 18 "ap not to rel/v.coarse sav ense uy duty, vapor barrier sh "LAY & some t, dense to v.c
Phot	os	Samp	es		Profile	
N 146 A6C1 Rm A3	8.9'	Tubes e 81/2 V 20 MB C 41/2- MB C 8/4-2	1- 20" -301/4" 81/4" 20"	Conc. Corc V Aricr	THE SA	ibar ND Blanket
L	]					······································





Room A31, AGC-1 - KR 06-03-17 (1)



Room A31, AGC-1 - KR 06-03-17 (2)





Room A31, AGC-1 - KR 06-03-17 (3)



Room A31, AGC-1 - KR 06-03-17 (4)





Room A31, AGC-1 - KR 06-03-17 (5)



Room A31, AGC-1 - KR 06-03-17 (6)





Room A31, AGC-1 - KR 06-03-17 (7)

Corin Project Locatic Total D	g No. Name: on: <u>Roc</u>	AGC Brid 31"	-2 geport Element All (class room Rg Type: 6" Core	Mach Est. Surface	File No. 05725-01 Sheet: Start Date: Juke 3 2017 Bevation:
Depth	Sample	Sample	Field De	escription	By: K. Rein
Feet	Туре	Depth	Subsurface Conditions: FO	RMATION: Classification, co	lor, moisture, tightness, etc.
			0-434" Conc Core ( #4 rebar w/in mid in N-S direction 43/4-7" SAND BLANKE tun moist (from @7" Yellow plastic possibly stepo U 7"-81/2" SAND BLAN 81/2-31" Fill silty and some graved	6"diam × 45% dle_third of s and 11" to 18" T SIHYSAND W coring_machi) / coring_machi) / coring	Min 5" Max thick (ab & speced = 18" apart apaint in E-W direction 1 some f. gravel/u.coarse 57AND Med donse irrier, heavy duty ble amounts of clay 2 to v. dense
	Photo	S	Samples		Profile

Photos	Samples	Profile
	Tubes e 81/2-16" 21-31" MBC 43/4-81/2" 81/2-21"	Sand blinket
American Geotechnical	Explanation: IIIIII Shelby	Medium Bag



Corir Project Location Total D	ig No. Name: In: <u>Ro</u> s	AGC- Brid	2 32 port Elementary School Steet Alf (classroom) Hatype 6" Core Mach Be suton Benetice:
Depth in Feet	Sample Type	Sample Depth	Field Description By: CP-
00		-	Subsurface Conditions FORMATION: Classification, color, moisture, lightness, etc.

Room A11, AGC-2 KR 06-03-17 (1)



Room A11, AGC-2 KR 06-03-17 (2)





Room A11, AGC-2 KR 06-03-17 (3)



Room A11, AGC-2 KR 06-03-17 (4)





Room A11, AGC-2 KR 06-03-17 (5)



Room A11, AGC-2 KR 06-03-17 (6)





Room A11, AGC-2 KR 06-03-17 (7)
	·,			(7, 2, 5, 0)
Coring No	AGC		File No. 🥘	5 7 2 3 - 01
Project Nam	ie: Bride	seport Flewant	Start Date: Ju	ne 3,2017
Location:	<u> Room Č</u>	1 (classroom)		
Total Depth	:28	" Rg Type: 6" Core	Mach. Est. Surface Elevation:	
Denth		Field D	escription By: /<	R
in Sam Feet Typ	ple Sample De Depth	Surface Conditions:		
		Subsurface Conditions: FC	DRMATION: Classification, color, moisture, tightr	ness, etc.
		0-5" Conc. Corc #14 rebur in mide e spaced 2 /8" and a/32" slab crack 5-63/4" SAND BCANK Med. brwn, Moiste e63/4 Henny duty Stego Wrap pr 63/4" = 8" SAND BCANK W/ = 1/32" dia 8-28" Fill silty SAN gravel med to	6" diam. × 4"/8" Min 5" Alle third of slab set on It in E-W direction & N- Hrough rebar location ET silly SAND W/some figravel, from corring: Machine), med. from corring: Machine), med. fellow plastic Mohst. Sarrici oduct ET same material as above uny i root underneath vapor D W/Variable amounts of e dk brwn SI moist to mois	Max thick rebarchair S'direction theoarse sand dense sheet possibly nor barrier sheet possibly nor barrier sheet possibly nor barrier
P	notos	Samples	Profile	
		MBC 5-8" 8-20'4" Tubes@ 8-16" 20'4-28"	Vapor Barrier	# 4 bar on chair Sand blanket
America Geotech	າ inical	Explanation: IIIIII Shelby	Fing Sampler   Medium Bag	162-3

i



	-	1			× ,
Corin Project Locatio Total D	g No. Name: on: <u>Ro</u> Depth:	AGC Bridg om C	-3 eport Fleme 2 (classroom) Rg Type: 6" G	re Mach. Est. Surface	File No. 057-25-01 Sheet:
Depth	Samola	Ormolo	Fie	ld Description	By: KR
	Туре	Depth .	Surface Conditions:	FORMATION: Classification, or	olor, moisture, tightness, etc.
Feet					

Room C1, AGC-3 - KR 6-3-17 (1)



Room C1, AGC-3 - KR 6-3-17 (2)





Room C1, AGC-3 - KR 6-3-17 (3)



Room C1, AGC-3 - KR 6-3-17 (4)





Room C1, AGC-3 - KR 6-3-17 (5)



Room C1, AGC-3 - KR 6-3-17 (6)





Room C1, AGC-3 - KR 6-3-17 (7)



Room C1, AGC-3 - KR 6-3-17 (8)





Room C1, AGC-3 - KR 6-3-17 (9)



Room C1, AGC-3 - KR 6-3-17 (10)

American Geotechnical, Inc. Project Name: Bridgeport Elementary School File No. 05725-01 Location: Jod area (see site map Boring No: AGHA-1 Total Depth: 10.1' Rig Type: Hand Auger = 4" diam. ETP Depth in Feet 0-0.5' Sod & Topsoil sandy LOAM, moist soft, abundant roots & organics dk brinn 0 Z A 0.5-6.5 Fill sity SANA w/ some gravel & cobbles sl. maist med. dense, slightly clayey at 5 to 6.5' 3 6.5-10,1' Silty SAND w/some clay and gravel moist med dense 0 5 3 \* perched ground water encountered at about 7' then becomes dryer (No groundwater) again 6 PART NUMBER AND (H<sub>2</sub>D Y with depth Le Perched Le Prouved Le Owater 7-Piezometer installed inside auger hole with: 8 6 screen interval from 4.4 to 10.1 solid / Non-screened interval from 0 to 4.4" 9-Sand pack from 1.5' to 10.1' Ð 10-Bentonite Seal from 10" to 18" Soil from 0 to 10" water tight cap & plastic irrigation cover Hzo e 7.6' depth after installation then piczometer was bailed Samples: T C 0.5-1.5' TC 7.5-8.0' LBC 0.5-5.0' 2.5-3.5' 5.0 - 6.0 6.5 - 7.0' 8.0 - 10.1





AGHA -1 - JP 6-3-17 (1)



AGHA -1 - JP 6-3-17 (2)





AGHA -1 - JP 6-3-17 (3)



AGHA -1 - JP 6-3-17 (4)





AGHA -1 - JP 6-3-17 (5)



AGHA -1 - JP 6-3-17 (6)





AGHA -1 - JP 6-3-17 (7)



AGHA -1 - JP 6-3-17 (8)





AGHA -1 - JP 6-3-17 (9)



AGHA -1 - JP 6-3-17 (10)





AGHA -1 - JP 6-3-17 (11)

American Geotechnical, Inc. Project Name: Bridgeport Elementary School File No. 05725-01 Location: Sod area (see site map Boring No: ABHA-Z Total Depth: \_\_\_\_\_ Rig Type: Hand Auger = 4" diam. Js Depth \_in Feet (W)(14/KA)FX/ 0-0.5' Topsoil + Sod sandy LOAM debrun moist soft 0.5-5.0' Fill silty SAND w/ some clay & gravel yellow-brown, med. dense, slightly moist, occasional sub-round cobbles to > 3.0" diam. 3 trace organics, refusal on large cobble 4 at 5.0' No groundwater encountered 5 Piezometer installed inside augerhale with: screen interval from 2.0'-5.0 solid / Non-screened interval from 0-2.0' sand pack from 1.5'- 5.0' Bentonite seal from 0.5 - 1.5' Soil from 0-0.5' Samples: Te 0.5-1.5' LBC 0.5-5.5' 2.0 - 2.4' 4.0 - 4.5' 5.0 - 5.5'



	Manager Colling	Americ	an Geote	chnical,	Inc.
FILE NO:	05725-01	PROJECT	BRIDGEPON	C ELEME	NTAFY
DESCRIP	TION: AGHA	-2			
DATE:	6/3/17	BY:	JEJJS		SHEET:
11					
1					
11					

AGHA-2 JP 6-3-17 (1)



AGHA-2 JP 6-3-17 (2)





AGHA-2 JP 6-3-17 (3)



AGHA-2 JP 6-3-17 (4)





AGHA-2 JP 6-3-17 (5)



AGHA-2 JP 6-3-17 (6)





AGHA-2 JP 6-3-17 (7)



### **APPENDIX E – LABORATORY TEST RESULTS**



### **APPENDIX E – LABORATORY TEST RESULTS**

### American Geotechnical, Inc. A;

**MOISTURE CONTENT / DRY DENSITY** 

Project Name	: Bridgepor	t Elementa	ry	2	ASTM D-221	6	La	b Manager:	RH	
File No	: 05725-01		·			-		Tested by	SA	
Date Sampled	: 6/3/2017							Date tested	6/5/2017	
	23570 Newball	23070 Nowball	23670	23070	23670	23570	23670	23670		230/0
Location	Ranch	Ranch	Ranch	Ranch	Ranch	Ranch	Ranch	Ranch	23670 Newhal	Newhall
	RD,Santa	RD,Santa	RD,Santa	RD,Santa	RD,Santa	RD,Santa	RD,Santa	RD,Santa	RD,Santa	RD,Santa
European Sec.	Clanta,CA	Clarita,CA	Clarita,CA	Clarita,CA	Clarita,CA	Clarita,CA	Clarita,CA	Clarita,CA	Clarita, CA	Clarita,CA
Excavation	AGHA-1	AGHA-1	AGHA-1	AGHA-1	AGHA-1	AGHA-1	AGHA-2	AGHA-2	AGHA-2	AGHA-2
Depth	0.5-1.5	2.5'-3.5'	4.5'-5'	6.5'-/'	7.5'-8'	9.1'-9.6'	0.5'-1.5'	2'-2.4'	4'-4.5'	5'-5.5'
	Gravish	Gravish Tar	Grayish	Olive Red	Gravish	Orangish	Gravish	Reddish/Gra	Deddich	Daddleb
Sail Description	Olive Tan-	Brown-	Orange	Brown-	Olive-Clayey	Gray Brown-	Olive Brown	v Olive-	Brown-	Brown-
	Clayey Sand	Clayey Sand	Clavey San	Clayey Sand	Sand w.	Sinty /Clayey	Clayey Sand	Clayey Sand	Clayey Sand	Clayey Sand
	w. Gravel	w. Gravel	w. Gravel	w. Gravel	Grave	Gravel	w. Gravel	w. Gravel	w. Gravel	w. Gravel
No of Rings (# or in )	6	1 3	1	6	5	0	0			
Ring Size (in )	25	2.5	25	25	25	25	25	2	4	0.5
Ring Weight (a)	143	1/12	1/3	1/3	142	4.0	2.0	2.5	2.5	2.5
RingWt +WetSoil (a)	1923	040.3	1224.5	1977	140	140	143	143	143	143
Total Ring Wt (g)	858.0	429.0	572 0	858.0	715.0	959.0	959 /	796.0	572.0	745.0
Wet Soil (a)	1065.0	520.3	652.5	1019.0	839.5	1037 7	1050.0	200.0	0/2.0 CAE 2	715.0
Volume (cf)	0.01704	0.00852	0.01136	0.01704	0.01420	0.01704	0.01704	0.00669	040.3	0.01400
Wet Density	137 75	134 60	126.60	131.80	130 30	124 22	120 00	122.04	0.01136	402.07
Cup No.	94	VO	C	10	Δ	511	130.30	100.91 N4	125.20	123.37
Cup+Wet Soil (a)	612 1	367.1	813.6	723.3	645.0	524.1	883.6	501.9	295.0	612.2
Cup+Dry Soil (a)	562.9	347.6	757.7	667.5	596.8	482.3	782.2	470.9	270 4	012.3 575.0
Moisture Loss (g)	49.20	19.50	55.90	55.80	48 20	41.80	81 40	31.00	15 50	26.70
	163.9	176.9	170.2	167.4	171.4	176.4	177 4	171.4	172.2	160.7
Dry Soil (a)	399.00	170.70	587.50	500 10	425.40	305.90	604.80	200 40	197 10	109.7
Moist, Content (%)	12.33	11.42	9.51	11.16	11.33	13.66	13 46	10 35	7 86	9.04
Dry Density (pcf)	122.63	120.80	115.60	118.57	117.04	118 09	120.73	121 35	116 07	3.04 113 14
Degree of Sat. (%)	89	78	56	72	70	86	92	72	47	50
	23670	23670	23870	23570	23870	20070	235/0	23571		
	Newhall	Newhail	Newhall	Newhall	Newhall	Newhall	Newhall	Newhall	23670 Newhall	Newhall
Location	Rench RD Sente	Ranch RD Sente	Ranch PD Santa	Ranch	Ranch	Ranch	Ranch	Ranch	Ranch	Ranch
	Clarita,CA	Clarite,CA	Clarita,CA	Clarita,CA	Clarita,CA	Clarita,CA	Clarita.CA	Clarita.CA	RU,Sama Clarita.CA	RU,Santa Ciarita CA
Excavation	AGCI-1	AGCI-1	AGCI-1	AGCI-1	AGCI-2	AGCI-2	AGCI-2	AGCI-2	AGCI-3	AGCI-3
Depth	8 1/2"-20"	20"-30 1/4"	4 1/2"-8 1/4"	8 1/4"-20"	8 1/2"-16"	21"-31"	4 3/4"-8 1/2"	8 1/2"-21"	8"-16"	20 1/4"-28"
Soil Description	Olive Brown- Silty Sand	Olive Brown Clayey Sand w.t Gravel	Olive Brown- Silty Sand	Med Brown- Silty Sand	Olive Brown Clayey Sand w. Gravel	Olive Brown Clayey Sand w. Gravel	Olive Brown Sillty Sand	Med Brown- Silty Sand w- Gravel	Olive Brown- Clayey Sand w. Gravel	Tanish Olive Clayey Sand w, Gravel
No. of Rings (# or in.)	6	6			5	6			6	5
Ring Size (in.)	2.5	2.5			2.5	2,5			2.5	2.5
Ring Weight (g)	143	143			142	440			143	143
RingWt.+WetSoil (g)	the second se	114	1	and the second s	140	143				
Total Dime \A/A /->	1915.4	1901.8			1579.4	143			1881.9	1611.7
Total Ring VVI. (g)	1915.4 858.0	1901.8 858.0			143 1579.4 715.0	143 1875.1 858.0			1881.9 858.0	<u>1611.7</u> 715.0
Wet Soil (g)	1915.4 858.0 1057.4	1901.8 858.0 1043.8			143 1579.4 715.0 864.4	143 1875.1 858.0 1017.1			1881.9 858.0 1023.9	1611.7 715.0 896.7
Vet Soil (g) Volume (cf)	1915.4 858.0 1057.4 0.01704	1901.8 858.0 1043.8 0.01704			143 1579.4 715.0 864.4 0.01420	143 1875.1 858.0 1017.1 0.01704			1881.9 858.0 1023.9 0.01704	1611.7 715.0 896.7 0.01420
Vet Soil (g) Volume (cf) Wet Density	1915.4 858.0 1057.4 0.01704 136.77	1901.8 858.0 1043.8 0.01704 135.01			143 1579.4 715.0 864.4 0.01420 134.17	143 1875.1 858.0 1017.1 0.01704 131.56			1881.9 858.0 1023.9 0.01704 132.44	1611.7 715.0 896.7 0.01420 139.18
Wet Soil (g) Volume (cf) Wet Density Cup No.	1915.4 858.0 1057.4 0.01704 136.77 1	1901.8 858.0 1043.8 0.01704 135.01 4	SH	VO	143 1579.4 715.0 864.4 0.01420 134.17 6	143 1875.1 858.0 1017.1 0.01704 131.56 SH	AS	HV	1881.9 858.0 1023.9 0.01704 132.44 200	1611.7 715.0 896.7 0.01420 139.18 12
Wet Soil (g) Volume (cf) Wet Density Cup No. Cup+Wet Soil (g)	1915.4 858.0 1057.4 0.01704 136.77 1 1018.3	1901.8 858.0 1043.8 0.01704 135.01 4 927.6	SH 588.1	VO 502.5	143 1579.4 715.0 864.4 0.01420 134.17 6 444.2	143 1875.1 858.0 1017.1 0.01704 131.56 SH 971.4	AS 583.9	HV 461.1	1881.9       858.0       1023.9       0.01704       132.44       200       459.9	1611.7 715.0 896.7 0.01420 139.18 12 613.9
Wet Soil (g) Volume (cf) Wet Density Cup No. Cup+Wet Soil (g) Cup+Dry Soil (g)	1915.4 858.0 1057.4 0.01704 136.77 1 1018.3 942.7	1901.8 858.0 1043.8 0.01704 135.01 4 927.6 857.9	SH 588.1 566.9	VO 502.5 472.8	143 1579.4 715.0 864.4 0.01420 134.17 6 444.2 419.3	143 1875.1 858.0 1017.1 0.01704 131.56 SH 971.4 896.0	AS 583.9 561.3	HV 461.1 435.1	1881.9       858.0       1023.9       0.01704       132.44       200       459.9       438.8	1611.7       715.0       896.7       0.01420       139.18       12       613.9       577.9
Vet Soil (g) Volume (cf) Wet Density Cup No. Cup+Wet Soil (g) Cup+Dry Soil (g) Moisture Loss (g)	1915.4 858.0 1057.4 0.01704 136.77 1 1018.3 942.7 75.60	1901.8 858.0 1043.8 0.01704 135.01 4 927.6 857.9 69.70	SH 588.1 566.9 21.20	VO 502.5 472.8 29.70	143 1579.4 715.0 864.4 0.01420 134.17 6 444.2 419.3 24.90	143 1875.1 858.0 1017.1 0.01704 131.56 SH 971.4 896.0 75.40	AS 583.9 561.3 22.60	HV 461.1 435.1 26.00	1881.9       858.0       1023.9       0.01704       132.44       200       459.9       438.8       21.10	1611.7       715.0       896.7       0.01420       139.18       12       613.9       577.9       36.00
Vet Soil (g) Volume (cf) Wet Density Cup No. Cup+Wet Soil (g) Cup+Dry Soil (g) Moisture Loss (g) Cup (g)	1915.4 858.0 1057.4 0.01704 136.77 1 1018.3 942.7 75.60 170.0	1901.8 858.0 1043.8 0.01704 135.01 4 927.6 857.9 69.70 164.4	SH 588.1 566.9 21.20 178.2	VO 502.5 472.8 <b>29.70</b> 176.9	143 1579.4 715.0 864.4 0.01420 134.17 6 444.2 419.3 24.90 166.7	143 1875.1 858.0 1017.1 0.01704 131.56 SH 971.4 896.0 75.40 178.2	AS 583.9 561.3 22.60 177.3	HV 461.1 435.1 <b>26.00</b> 178.0	1881.9       858.0       1023.9       0.01704       132.44       200       459.9       438.8       21.10       164.9	1611.7       715.0       896.7       0.01420       139.18       12       613.9       577.9       36.00       165.9
Vet Soil (g) Volume (cf) Wet Density Cup No. Cup+Wet Soil (g) Cup+Dry Soil (g) Moisture Loss (g) Cup (g) Dry Soil (g)	1915.4 858.0 1057.4 0.01704 136.77 1 1018.3 942.7 75.60 170.0 772.70	1901.8 858.0 1043.8 0.01704 135.01 4 927.6 857.9 69.70 164.4 693.50	SH 588.1 566.9 21.20 178.2 388.70	VO 502.5 472.8 29.70 176.9 295.90	143 1579.4 715.0 864.4 0.01420 134.17 6 444.2 419.3 24.90 166.7 252.60	143 1875.1 858.0 1017.1 0.01704 131.56 SH 971.4 896.0 75.40 178.2 717.80	AS 583.9 561.3 22.60 177.3 384.00	HV 461.1 435.1 26.00 178.0 257.10	1881.9       858.0       1023.9       0.01704       132.44       200       459.9       438.8       21.10       164.9       273.90	1611.7       715.0       896.7       0.01420       139.18       12       613.9       577.9       36.00       165.9       412.00
Wet Soil (g) Wet Soil (g) Volume (cf) Wet Density Cup No. Cup+Wet Soil (g) Cup+Dry Soil (g) Moisture Loss (g) Cup (g) Dry Soil (g) Moist. Content (%)	1915.4 858.0 1057.4 0.01704 136.77 1 1018.3 942.7 75.60 170.0 772.70 9.78	1901.8       858.0       1043.8       0.01704       135.01       4       927.6       857.9       69.70       164.4       693.50       10.05	SH 588.1 566.9 21.20 178.2 388.70 5.45	VO 502.5 472.8 29.70 176.9 295.90 10.04	143 1579.4 715.0 864.4 0.01420 134.17 6 444.2 419.3 24.90 166.7 252.60 9.86	143 1875.1 858.0 1017.1 0.01704 131.56 SH 971.4 896.0 75.40 178.2 717.80 10.50	AS 583.9 561.3 22.60 177.3 384.00 5.89	HV 461.1 435.1 26.00 178.0 257.10 10.11	1881.9       858.0       1023.9       0.01704       132.44       200       459.9       438.8       21.10       164.9       273.90       7.70	1611.7     715.0     896.7     0.01420     139.18     12     613.9     577.9     36.00     165.9     412.00     8.74
Wet Soil (g) Wet Soil (g) Volume (cf) Wet Density Cup No. Cup+Wet Soil (g) Cup+Dry Soil (g) Moisture Loss (g) Cup (g) Dry Soil (g) Moist. Content (%) Dry Density (pcf)	1915.4 858.0 1057.4 0.01704 136.77 1 1018.3 942.7 75.60 170.0 772.70 9.78 124.58	1901.8       858.0       1043.8       0.01704       135.01       4       927.6       857.9       69.70       164.4       693.50       10.05       122.68	SH 588.1 566.9 21.20 178.2 388.70 5.45	VO 502.5 472.8 29.70 176.9 295.90 10.04	143     1579.4     715.0     864.4     0.01420     134.17     6     444.2     419.3     24.90     166.7     252.60     9.86     122.13	143 1875.1 858.0 1017.1 0.01704 131.56 SH 971.4 896.0 75.40 178.2 717.80 10.50 119.05	AS 583.9 561.3 22.60 177.3 384.00 5.89	HV 461.1 435.1 26.00 178.0 257.10 10.11	1881.9       858.0       1023.9       0.01704       132.44       200       459.9       438.8       21.10       164.9       273.90       7.70       122.97	1611.7     715.0     896.7     0.01420     139.18     12     613.9     577.9     36.00     165.9     412.00     8.74

22725 Old Canal Road, Yorba Linda, CA 92897 - (714) 885-3900 - FAX (714) 885-3909 2640 Financial Court, Suite A, San Diego, CA 92117 - (858) 450-460 - FAX (658) 457-0814 3100 File Circle, Suite 103, Sacramento, CA 95827 - (916) 388-2088 - FAX (916) 308-2188 5800 Spring Mountain Road, Suite 201, Las Vegas, NV 89145 - (702) 562-5048 - FAX (702) 562-2457



#### **MOISTURE CONTENT / DRY DENSITY**

Project Name:	Bridgeport	t Elementar	у	ASTM D-221	6	La	b Manager:	RH	
File No:	05725-01						Tested by:	SA	
Date Sampled:	6/3/2017						Date tested:	6/5/2017	
	Newball	23670 Newball			1	T	T	1	1
Location	Ranch	Ranch			1				1
	RD,Santa	RD,Santa			-	-			
(Furner allow)	Clanta,CA	Clarita,CA		 					
Excavation	AGCI-3	AGCI-3		 					1
Depth	5"-8"	8"-20 1/4"		 					
Soil Description	Olive Brown Silty Sand	Med Brown- Silty Sand w. Gravel							
INO. OF KINGS (# OF IN.)				 		1			
Ring Size (in.)				 	No. No.				
Ring Weight (g)									
RingWt.+WetSoil (g)				 		-			
Total Ring Wt. (g)									
Wet Soil (g)				 					
Volume (cf)									
Wet Density				 					
Cup No.	200	N			1			81	
Cup+Wet Soil (g)	444.6	567.2							
Cup+Dry Soil (g)	431.3	535.6							
Moisture Loss (g)	13.30	31.60		 				_	
Cup (g)	164.9	169.4							
Dry Soil (g)	266.40	366.20							
Moist. Content (%)	4.99	8.63							
Dry Density (pcf)									[]
Degree of Sat. (%)	#VALUE!	#VALUE!							[
Location			T			r	1		1 1
Excavation				 -				-	
Depth	1								
Soil Description									
No. of Rings (# or in.)									
Ring Size (in.)									
Ring Weight (g)									
RingWt,+WetSoil (g)						1			
Total Ring Wt. (g)									
Wet Soil (g)									
Volume (cf)									
Wet Density			1						
Cup No.			1						
Cup+Wet Soil (a)									
Cup+Dry Soil (a)									
Moisture Loss (a)									
Cup (g)				 					
Dry Soil (a)				 					
Moist, Content (%)				 					
Dry Density (pcf)				 					
Degree of Sat. (%)				 					

Assumes S.G. of 2.7





#### PARTICLE SIZE ANALYSIS

ASTM D422 (Over #4)

Project Name: Bridgeport Elementary Location: 23670 Newhall Ranch Rd. Santa Clarita,CA File No: 05725-01 Date: 6/15/2017

Excavation: AGHA-1 Depth: 0,5'-5' By: RH

Total Weight of Sample	699.6 g
Dry Weight After Moisture Corr.	674.1 g

Sieve Size	Wet Retained	ained Wet Retained % Re		Retained Accumulated	Passing %	
	(g)	(g)		%	100.00	
3 "						
2 1/2 "						
2 "			Contraction of the			
1 1/2 "	0.0	0.0	0.0	0.0	100.0	
1 "	0.0	0.0	0.0	0.0	100.0	
3/4 "	0.0	0.0	0.0	0.0	100.0	
1/2 "	3.3	3.3	0.5	0.5	99.5	
3/8 "	10.9	14.2	1.6	2.1	97.9	
#4	23.7	37.9	3.5	5.6	94.4	
#8						
# 16						
# 30						
# 40						
# 50						
# 60						
# 100						
# 140						
# 200						
PAN	636.2	674.1	94.4	100.0	0.0	



### PARTICLE SIZE ANALYSIS FOR HYDROMETER

ASTM D-422 (Under #4)

Project Name: Bridgeport Elementary

Location: 23670 Newhall Ranch Rd. Santa Clarita,CA File No: 05725-01 Date: 6/15/2017 Excavation: AGHA-1 Depth: 0.5'-5' By: RH

#### **Moisture** Correction

Wet Weight + Tare	827.1
Dry Weight + Tare	803
Moisture Weight	24.1
Tare	166.8
Dry Soil Weight	636.2
Moisture Content	3.8
% passing #4 sieve	94

Percent Passing #200 36.00

Sieve Size	Retained	Accumulated Retained	Retained	Accumulated	Passing	Corrected Passing
	(g)	(g)	%	%	%	%
3"						
2 1/2 "						
2"						
1 1/2 "			-			1
1"					6	1
3/4 "						1
3/8 "						
1/2 "						
#4					100.00	
#8	30.6	30.6	4.81	4.81	95.19	89.84
# 16	51.4	82	8.08	12.89	87.11	82.21
# 30	69.9	151,9	10.99	23.88	76.12	71.84
# 40						1
# 50	91.5	243.4	14.38	38.26	61.74	58.27
# 60				-		
# 100	96.7	340.1	15.20	53,46	46.54	43.93
# 140						1.0.00
# 200	53.4	393.5	8.39	61.85	38.15	36.00
PAN	242.7	636.2	38.15	100.00	0.00	0.00

22725 Old Canal Road, Vorba Linda, CA 92887 - (714) 685-3900 - FAX (714) 685-3909 2640 Financial Court, Suite A, San Diego, CA 92137 - (859, 450-4040 - FAX (858), 457-0814 3100 Fite Circle, Suite 103, Sacramento, CA 95827 - (916) 268-2088 - FAX (915) 268-2188 5500 Spring Mountain Road, Suite 201, Las Vegas, IVV 89146 - (702) 562-5046 - FAX (702) 562-2457



### **HYDROMETER TEST**

ASTM D-422

Project Name: Bridgeport Elementary Location: 23670 Newhall Ranch Rd. Santa Clarita,CA File No: 05725-01 Date: 6/15/2017

Excavation: AGHA-1 Depth: 0.5'-5' By: RH

		1				the second se	Address of the local data and th
Date	6/14/2017	6/14/2017	6/14/2017	6/14/2017	6/14/2017	6/14/2017	6/15/2017
Time	11:30	11:33	11.43	11:58	12:28	3:38	11:28
Elapsed Time (min)	2	5	15	30	60	250	1440
Hydrometer 152 H Reading							
A	21	18	16	15	14	12	11
В	5	5	5	5	5	5	5
А-В	16	13	11	10	9	7	6
D (Table 1)	0.99	0.99	0.99	0.99	0.99	0.99	0.99
E - Soit In Solution*100	27.37	22.24	18.82	17.11	15.40	11.98	10.27
Corrected Grading	25.83	20.99	17.76	16.15	14.53	11.30	9.69
F % Passing # 4 Sieve	94.38	94.38	94.38	94.38	94.38	94.38	94.38
Temp C	22	22	22	22	22	22	22
G =Eff, Depth (Table 2)	12.9	13.3	13.7	13.8	14	14.3	14.5
Table 3	0.01312	0.01312	0.01312	0.01312	0.01312	0.01312	0.01312
Diameter of Particle (mm)	0.0333	0.0214	0.0125	0.0089	0.0063	0.0031	0.0013
Soil Moisture							
L= Wt. wet soil + tare (g)	100.13	100.13	100.13	100.13	100.13	100.13	100.13
M= Wt. dry soil + tare (g)	97.59	97.59	97.59	97.59	97.59	97.59	97.59
N= Wt. of tare (g)	31.49	31.49	31.49	31.49	31.49	31.49	31.49
O= Wt. of moisture loss (g)	2.54	2.54	2.54	2.54	2.54	2.54	2.54
P= Wt of dry soil (g)	66.1	66.1	66.1	66.1	66.1	66.1	66.1
Q= Moisture Content %	3.84	3.84	3.84	3.84	3.84	3.84	3.84
Soil Weight							
R= Specific Gravity	2.7	2.7	2.7	2.7	2.7	2.7	2.7
S= Wet Soil (g)	60.09	60.09	60.09	60.09	60.09	60.09	60.09 -
T= Dry Soil (g)	57.87	57.87	57.87	57.87	57.87	57.87	57.87





### PARTICLE SIZE ANALYSIS

ASTM D422 (Over #4)

Project Name: Bridgeport Elementary Location: 23670 Newhall Ranch Rd. Santa Clarita,CA File No: 05725-01 Date: 6/15/2017

Excavation: AGHA-1 Depth: 5'-8' By: RH

Total Weight of Sample	764.1 g
Dry Weight After Moisture Corr.	742.8 g

Sieve Size	Wet Retained	Accumulated Wet Retained % Retained		Retained Accumulated	Passing %	
	(9)	(g)		%	100.00	
3 "						
2 1/2 "						
2 "						
1 1/2 "	0.0	0.0	0.0	0.0	100.0	
1 "	0.0	0.0	0.0	0.0	100.0	
3/4 "	0.0	0.0	0.0	0.0	100.0	
1/2 "	10.8	10.8	1.5	1.5	98.5	
3/8 "	3.6	14.4	0.5	1.9	98.1	
#4	25.9	40.3	3.5	5.4	94.6	
#8						
# 16						
# 30						
# 40						
# 50						
# 60						
# 100						
# 140						
# 200						
PAN	702.5	742.8	94.6	100.0	0.0	

22725 Old Canal Road. Yorba Linda, CA 92887 - (714) 685-3900 - FAX (714) 685-3909 2640 Financial Court, Surte A. San Diego. CA 92117 - (858) 450-4040 - FAX (858) 457-0814 3100 Fite Circle, Surte 103, Sacramento, CA 95827 - (916) 368-2088 - FAX (916) 368-2188 5600 Spring Mountain Road. Surte 201, Las Vegas, NV 89146 - (702) 562-5046 - FAX (702) 562-2457



### PARTICLE SIZE ANALYSIS FOR HYDROMETER

ASTM D-422 (Under #4)

Project Name: Bridgeport Elementary Location: 23670 Newhall Ranch Rd. Santa Clarita,CA File No: 05725-01 Date: 6/15/2017

Excavation: AGHA-1 Depth: 5'-8' By: RH

#### **Moisture Correction**

Wet Weight + Tare	898.5
Dry Weight + Tare	878.4
Moisture Weight	20.1
Tare	175.9
Dry Soil Weight	702.5
Moisture Content	2.9
% passing #4 sieve	95

Percent Passing #200 32.97

Sieve Size	Retained	Accumulated Retained	Retained	Accumulated	Passing	Corrected Passing
	(g)	(g)	%	%	%	%
3 "				1		
2 1/2 "						1
2 "						
1 1/2 "			- 16			
1"						
3/4 "						1
3/8 "						
1/2 "						1
#4					100.00	
#8	40.1	40.1	5.71	5.71	94.29	89.18
# 16	60.2	100.3	8.57	14.28	85.72	81.07
# 30	81.1	181.4	11.54	25.82	74.18	70.15
# 40						
# 50	117.7	299.1	16.75	42.58	57.42	54.31
# 60						
# 100	107.1	406.2	15.25	57.82	42.18	39.89
# 140						
# 200	51.4	457.6	7.32	65.14	34.86	32.97
PAN	244.9	702.5	34.86	100.00	0.00	0.00



#### **HYDROMETER TEST**

ASTM D-422

Project Name: Bridgeport Elementary Location: 23670 Newhall Ranch Rd. Santa Clarita,CA File No: 05725-01 Date: 6/15/2017

Excavation: AGHA-1 Depth: 5'-8' By: RH

		r			the second s	14 have 10 hav	
Date	6/14/2017	6/14/2017	6/14/2017	6/14/2017	6/14/2017	6/14/2017	6/15/2017
Time	11:18	11:21	11:31	11:46	12:16	3:26	11.16
Elapsed Time (min)	2	5	15	30	60	250	1440
Hydrometer 152 H Reading				•			
A	21	19	17	16	15	13	11
В	5	5	5	5	5	5	5
A-B	16	14	12	11	10	8	6
D (Table 1)	0.99	0.99	0.99	0,99	0.99	0.99	0.99
E - Soil In Solution*100	27.16	23.77	20.37	18.67	16.98	13.58	10.19
Corrected Grading	25.69	22.48	19.27	17.66	16.05	12.84	9.63
F % Passing # 4 Sieve	94.57	94.57	94.57	94.57	94.57	94.57	94.57
Temp C	22	22	22	22	22	22	22
G =Eff. Depth (Table 2)	12.9	13.2	13.3	13.7	13.8	14.2	14.5
Table 3	0.01312	0.01312	0.01312	0.01312	0.01312	0.01312	0.01312
Diameter of Particle (mm)	0.0333	0.0213	0.0124	0.0089	0.0063	0.0031	0.0013
Soil Moisture				I		0.0001	0.0010
L= Wt. wet soil + tare (g)	100.53	100.53	100.53	100.53	100 53	100.53	100.53
M= Wt. dry soil + tane (g)	98.56	98.56	98,56	98.56	98.56	98.56	98.56
N= Wt. of tare (g)	31.38	31.38	31.38	31.38	31.38	31.38	31 38
O= Wt. of moisture loss (g)	1.97	1.97	1.97	1.97	1.97	1.97	1.00
P= Wt of dry soil (g)	67.18	67.18	67.18	67.18	67.18	67 18	67 18
Q= Moisture Content %	2.93	2.93	2.93	2.93	2.93	293	2.93
Soil Weight							2.00
R= Specific Gravity	2.7	2.7	2.7	2.7	2.7 1	27	27
S= Wet Soil (g)	60.03	60.03	60.03	60.03	60.03	60.03	60.03
T= Dry Soil (g)	58.32	58.32	58.32	58.32	58.32	58.32	58.32
	the second se	the second se				00.02	OO.OL

22725 Old Canal Road, Yorba Linda, CA 92887 - (714) 585-3900 - FAX (714) 585-3909 2640 Financial Courl, Suite A, San Diego, CA 92117 - (858) 450-4040 - FAX (858) 457-0814 2100 Frie Cricle, Suite 103, Sacramento, CA 95827 - (916) 388-2088 - FAX (915) 388-2188 5600 Spring Mountain Road, Suite 201, Las Vegas, NV 89146 - (702) 562-5048 - FAX (702) 562-2457





#### PARTICLE SIZE ANALYSIS FOR HYDROMETER

ASTM D-422 (Under #4)

Project Name: Bridgeport Elementary Location: 23670 Newhall Ranch Rd. Santa Clarita,CA File No: 05725-01 Date: 6/15/2017 Excavation: AGHA-2 Depth: 0.5'-5.5' By: RH

#### **Moisture** Correction

Wet Weight + Tare	949.6
Dry Weight + Tare	928.5
Moisture Weight	21.1
Tare	160.7
Dry Soil Weight	767.8
Moisture Content	2.7
% passing #4 sieve	96

Percent Passing #200 33.36

Sieve Size	Retained	Accumulated Retained	Retained	Accumulated	Passing	Corrected Passing
	(g)	(g)	%	%	%	%
3 "						-
2 1/2 "						
2 "						
1 1/2 "					4	
1"						
3/4 "						
3/8 "						1
1/2 "						1
#4					100.00	
#8	37.9	37.9	4.94	4.94	95.06	90.85
# 16	64.6	102.5	8.41	13.35	86.65	82.81
# 30	85.2	187.7	11.10	24.45	75.55	72.21
# 40						
# 50	118.9	306.6	15.49	39.93	60.07	57.41
#60						
# 100	132.8	439.4	17.30	57.23	42.77	40.88
# 140						
# 200	60.4	499.8	7.87	65.10	34.90	33.36
PAN	268.0	767.8	34.90	100.00	0.00	0.00

22725 Old Canal Road, Yolba Linda, CA 92887 - (714) 685-3900 - FAX (714) 685-3909 2640 Financial Court, Suite A. San Diego, CA 92317 - (858) 450-4040 - FAX (858) 457-0814 3100 File Circle, Suite 103, Saciamento, CA 95827 - (916) 368-2088 - FAX (916) 368-2188 5600 Spring Mountain Road, Suite 201, Las Vegas, NV 89146 - (702) 562-5046 - FAX (702) 562-2457



### PARTICLE SIZE ANALYSIS

ASTM D422 (Over #4)

Project Name: Bridgeport Elementary Location: 23670 Newhall Ranch Rd. Santa Clarita,CA File No: 05725-01 Date: 6/15/2017

Excavation: AGHA-2 Depth: 0.5'-5.5' By: RH

Total Weight of Sample	825.5 g
Dry Weight After Moisture Corr.	803.4 g

Sieve Size	Wet Retained	Accumulated Wet Retained	% Retained	Retained Accumulated	Passing %
	(9)	(g)		%	100.00
3 "					
2 1/2 "					
2 "					
1 1/2 "	0.0	0.0	0.0	0.0	100.0
1 "	0.0	0.0	0:0	0.0	100.0
3/4 "	0.0	0.0	0.0	0.0	100.0
1/2."	0.0	0.0	0.0	0.0	100.0
3/8 "	2.9	2.9	0.4	0.4	99.6
#4	32.7	35,6	4.1	4.4	95.6
#8					
#16					
# 30			1		
# 40					
# 50					
# 60					
# 100					
# 140					
# 200					
PAN	767.8	803.4	95.6	100.0	0.0



#### **HYDROMETER TEST**

ASTM D-422

Project Name: Bridgeport Elementary Location: 23670 Newhall Ranch Rd. Santa Clarita,CA File No: 05725-01 Date: 6/15/2017 Excavation: AGHA-2 Depth: 0.5'-5.5' By: RH

Date	6/14/2017	6/14/2017	6/14/2017	6/14/2017	6/14/2017	6/14/2017	6/15/2017	
Time	11:06	11:09	11:19	11:34	12:04	3:14	11:04	
Elapsed Time (min)	2	5	15	30	60	250	1440	
Hydrometer 152 H Reading								
A	21	19	17	16	15	13	11	
В	5	5	5	5	5	5	5	
А-В	16	14	12	11	10	8	6	
D (Table 1 )	0,99	0.99	0.99	0.99	0.99	0.99	0.99	
E - Soit In Solution*100	27.12	23.73	20.34	18.64	16.95	13.56	10.17	
Corrected Grading	25.92	22.68	19.44	17.82	16.20	12.96	9.72	
F % Passing # 4 Sieve	95.57	95.57	95.57	95.57	95.57	95.57	95.57	
Temp C.	22	22	22	22	22	22	22	
G =Eff. Depth (Table 2)	12.9	13.2	13.5	13.7	13.8	14.2	14.5	
Table 3	0.01312	0.01312	0.01312	0.01312	0.01312	0.01312	0.01312	
Diameter of Particle (mm)	0.0333	0.0213	0.0124	0.0089	0.0063	0.0031	0.0013	
Soil Moisture					ň.			
L= Wt. wet soil + tare (g)	100.7	100.7	100.7	100.7	100.7	100.7	100.7	
M≃ Wt. dry soil + tare (g)	98.83	98.83	98.83	98.83	98.83	98.83	98.83	
N= Wt. of tane (g)	31.37	31.37	31.37	31.37	31.37	31.37	31.37	
O= Wt. of moisture loss (g)	1.87	1.87	1.87	1.87	1.87	1.87	1.87	
P= Wt of dry soil (g)	67.46	67.46	67.46	67.46	67.46	67.46	67.46	
Q= Moisture Content %	2.77	2.77	2.77	2.77	2.77	2.77	2.77	
Soil Weight								
R= Specific Gravity	2.7	2.7	2.7	2.7	2.7	2.7	2.7	
S= Wet Soil (g)	60.03	60.03	60.03	60.03	60.03	60.03	60.03	
T= Dry Soil (g)	58.41	58.41	58.41	58.41	58.41	58.41	58.41	

22725 Ołd Canal Road, Yorba Linda: CA 92887 - (714) 685-3900 - FAX (714) 685-3909 2640 Financial Court, Suite A, San Diego, CA 92117 - (858) 450-4040 - FAX (858) 457-0914 3100 Frie Circle, Surte 103, Sacramento, CA, 95827 - (916) 368-2088 - FAX (916) 368-2188 5600 Spring Nountain Road, Surte 201, Las Vegas, NV 89146 - (702) 562-5048 - FAX (702) 562-24457 American Geotechnical Protecting Your Future

CORE MEASUREMENTS

ASTM C174-87

F.N. 05725-01	PROJECT BRIDE POR	ELENT SEH
ADDRESS _2-3670 New	hall Ranch Road, Souta Chrite	a,cA
AG 6-1 DA	TE CORED _6/3/2017	AG REP_ICZ
DATE MEASURED	ROOM DOTHER BY SA	
MEASUREMENT LOCATION	MEASUREMENT INCREMENTS	LENGTH (INCHES)
1	CORE CENTER	4.69
2	0*	4.90
3	45°	4.90
4	90°	4.83
5	135'	4.77
6	180*	5.07
7	225'	5.27
8	270'	5.06
9	315*	4.96
Α'	VERAGE LENGTH (INCHES)	4.9

• CORE MEASUREMENTS WERE TAKEN AT 45 DEGREE INCREMENTS #2 ON CORE'S SMOOTHER INDICATES STARTING POINT (0 DEGREES) ROTATION WAS ACCOMPLISHED IN A CLOCKWISE DIRECTION WITH REFERENCE TO THE SMOOTHER END



### American Geotechnical, Inc.

File No. 5725-01 Bridgeport Elementary School

|--|--|

23670 Newhall Ranch Road- SA 6-9-17 (1)

	AMERICAN	
5	Geottechnical, INC.     Project:   Geottechnical, INC.     Date:   Geottechnical, INC.     Date:   Geottechnical, INC.     Frame:   Z     By:   SA     Address:   Addc-1	

23670 Newhall Ranch Road- SA 6-9-17 (2)
MERICAN GEOTECHNICAL, INC. Project: Benog & Part Safon Scall Date: CAS Rep File No.: 572550 Frame, BySA

23670 Newhall Ranch Road- SA 6-9-17 (3)

Project: <u>Del Del Plant</u> <u>Submit Sch</u> Date: <u>G/9   Lan</u> <u>File No.: 5725-01</u> <u>Prame:</u> <u>4</u> <u>By:</u> <u>5A</u> <u>Address:</u> <u>AGC-1</u> <u>CARBONATION</u>	
CARDINATION	

23670 Newhall Ranch Road- SA 6-9-17 (4)

Merican Geotechnical Protecting Your Future

CORE MEASUREMENTS

ASTM C174-87

F.N. 05725-01 ADDRESS _ 23670 NO	PROJECT BRIDEPORT	ELEM SCH.
AG C-Z DA	AGREP KR	
DATE MEASURED_G	16/2017 BY 5-	<i>t</i>
MEASUREMENT LOCATION MEASUREMENT INCREMENTS		LENGTH (INCHES)
1	CORE CENTER	4.81
2	0'	4.48
3	45'	4.72
4	90*	4.78
5	135'	4.92
6	180°	4,98
7	225'	4.75
8	270'	4.85
9	315*	4.74
AVERAGE LENGTH (INCHES)		4.8

• CORE MEASUREMENTS WERE TAKEN AT 45 DEGREE INCREMENTS #2 ON CORE'S SMOOTHER INDICATES STARTING POINT (0 DEGREES) ROTATION WAS ACCOMPLISHED IN A CLOCKWISE DIRECTION WITH REFERENCE TO THE SMOOTHER END

	°( 7	5	-kaman	c			SP7	INC
Г	9	8	7	6	5	4	3	2
		Phin 14	12.45	Q	And 16 CI S	2.69 N	Polie 1/2 O	jaz,
					-4/2/		11.11	]

	AMERICAN GEOTECHNICAL, INC. Project: <u>Belog &amp; Rest &amp; Belog &amp; Col</u> Date: <u>C.M. File No.: 5725-01</u> Frame: <u>5</u> By: <u>5A</u> Address: <u>AGC-2 RMAII</u>
N. W.	

23670 Newhall Ranch Road- SA 6-9-17 (5)

2 61	AMERICAN GEOTECHNICAL, INC. Project: Devoce Port Electic Soft Date: 6/9 12017 File No.: 5725-0/ Frame: 6 By: 54 Address: AGC-2 RMAIL

23670 Newhall Ranch Road- SA 6-9-17 (6)

File No. 5725-01 Bridgeport Elementary School

AMERICAN GEOTECHNICAL, INC. Project: ALIOGE RET ELEM SCH Date: G/9 Izon File No.: 57259 Frame: 7 By: SA Address: AGC-2 RMAIL

23670 Newhall Ranch Road- SA 6-9-17 (7)

	AMERICAN
	Date: 6/9 2017 File No.: 5725-0/
0.2	Address: AGC-2 RMAIL CARBONATION

23670 Newhall Ranch Road- SA 6-9-17 (8)

Protecting Your Future

ASTM C174-87

CORE MEASUREME	NTS	
F.N. 05725-01	PROJECT PALIGEPOR	telern. sell.
ADDRESS ( R	n(-1)	
AG	DATE CORED 613/2017	AGREPER
	MILY ROOM BOTHER BY	S K
MEASUREMENT LOCAT	ION MEASUREMENT INCREMENTS	LENGTH (INCHES)
1	CORE CENTER	4.94
2	0*	4.04
3	45'	4.63
4	90*	4,61
5	135'	4.56
6	180'	4.67
7	225*	4.86
8	270°	4,85
9	315*	4.31
	AVERAGE LENGTH (INCHES)	4.6

· CORE MEASUREMENTS WERE TAKEN AT 45 DEGREE INCREMENTS #2 ON CORE'S SMOOTHER INDICATES STARTING POINT (0 DEGREES) BOTATION WAS ACCOMPLISHED IN A CLOCKWISE DIRECTION WITH REFERENCE TO THE SMOOTHER END

1/64 B C Kell	CORE DIAMETE	ER	5.7	INCHES
9 8 7 6 2 54 prov prov 2 00 1/2" 3160 1/2" 1/2" 1/2" 1/2" 1/2" 1/2" 1/2" 1/2" 1/2" 1/2"	5 2.54 PRM	4	3 2 Mc Root Vice Const	3/64
REINFORCEMENT: WIRE MESH BREBAR		_ BUBBLES	1/2 (YES)	
membranie - STEIENO 4	alow 15	whit	HAPID	Cut

A	American	Geotec	hnical	Inc.
-0-	CHOTECHING AL ENGINEE	BING J MALLBOALS	TRATING & IN	SPECTRUM

Address:     Address:
Frame: By: Address: 

23670 Newhall Ranch Road- SA 6-9-17 (9)

Add
Rm c-I

## 23670 Newhall Ranch Road- SA 6-9-17 (10)

File No. 5725-01 Bridgeport Elementary School

MERICAN   GEOTECHNICAL, INC.

23670 Newhall Ranch Road- SA 6-9-17 (11)

AMERICAN   Broject:   Bate:   CARBONATION

23670 Newhall Ranch Road- SA 6-9-17 (12)

